

- 2.11.  $\epsilon_{AB} = \frac{0,5 \Delta L}{L}$
- 2.13.  $(\gamma_C)_{xy} = -11,6(10^{-3}) \text{ rad},$   
 $(\gamma_D)_{xy} = 11,6(10^{-3}) \text{ rad}$
- 2.14.  $\epsilon_{AC} = 1,60(10^{-3}) \text{ mm/mm},$   
 $\epsilon_{DB} = 12,8(10^{-3}) \text{ mm/mm}$
- 2.15.  $\epsilon_{AB} = 16,8(10^{-3}) \text{ m/m}$
- 2.16.  $(\gamma_{nt})_A = 0,05024 \text{ rad}, (\gamma_{nt})_B = 0,05024 \text{ rad}$
- 2.17.  $\epsilon_{AB} = -4,686 \times 10^{-3} \text{ mm/mm},$   
 $\epsilon_{AC} = 20,000 \times 10^{-3} \text{ mm/mm},$   
 $\epsilon_{DB} = -30,000 \times 10^{-3} \text{ mm/mm},$
- 2.18.  $\epsilon_{AB} = 1,61(10^{-3}) \text{ mm/mm},$   
 $\epsilon_{CD} = 126(10^{-3}) \text{ mm/mm}$
- 2.19.  $(\gamma_A)_{xy} = -0,0262 \text{ rad}, (\gamma_B)_{xy} = -0,205 \text{ rad},$   
 $(\gamma_C)_{xy} = 0,205 \text{ rad}, (\gamma_D)_{xy} = 0,0262 \text{ rad}$
- 2.21.  $\epsilon = 2kx$
- 2.22.  $\gamma_{xy} = -0,0200 \text{ rad}$
- 2.23.  $\gamma_{xy} = 0,02 \text{ rad}$
- 2.25.  $\gamma_{xy} = 0,0142 \text{ rad}$
- 2.26.  $\epsilon_{DB} = -0,00680 \text{ mm/mm},$   
 $\epsilon_{AD} = 0,0281(10^{-3}) \text{ mm/mm}$
- 2.27.  $\epsilon_x = 0, \epsilon_y = 0,00319, \gamma_{xy} = 0,0798 \text{ rad},$   
 $\epsilon_{BE} = -0,0179 \text{ mm/mm}$
- 2.29.  $(\gamma_C)_{xy} = -0,137 \text{ rad}, (\gamma_D)_{xy} = 0,137 \text{ rad}$
- 2.30.  $\Delta y = 2,03 \text{ mm}$
- 2.31.  $\Delta L = 30,00 \text{ mm}$
- 2.33.  $\Delta L = 42,252 \text{ mm}$
- 2.34.  $\epsilon_{AB} = \frac{v_B \text{ sen } \theta}{L} - \frac{u_A \text{ cos } \theta}{L}$

Capítulo 3

- 3.1.  $E_{\text{aprox}} = 26,67 \text{ GPa}$
- 3.2.  $E_{\text{aprox}} = 387,3 \text{ GPa}, u_r = 0,0697 \text{ MJ/m}^3$
- 3.3.  $u_t = 0,595 \text{ MJ/m}^3$
- 3.4.  $E_{\text{aprox}} = 260,8 \text{ GPa}, \sigma_e = 448 \text{ MPa},$   
 $\sigma_{\text{lim}} = 890 \text{ MPa}, \sigma_R = 753,8 \text{ MPa}$
- 3.5.  $E = 290 \text{ GPa}, P_e = 32,80 \text{ kN}, P_{\text{máx}} = 62,20 \text{ kN}$
- 3.6.  $E = 290 \text{ GPa}, \text{Valor}_{\text{RE}} = 0,08621 \text{ mm},$   
 $\text{Valor}_{\text{ps}} = 3,91379 \text{ mm}$
- 3.7.  $u_r = 0,145 \text{ MPa}, u_t = 132 \text{ MPa}$
- 3.9.  $E = 38,5 \text{ GPa}, u_r = 77,00 \text{ MPa}, u_t = 134,75 \text{ MPa}$
- 3.10.  $L = 1.250,363 \text{ mm}$
- 3.11.  $L = 254,143 \text{ mm}$

- 3.13.  $\Delta P = 220,22 \text{ kN}$
- 3.14.  $E = 766,3 \text{ MPa}$
- 3.15.  $A_{\text{exig}} = 150 \text{ mm}^2, P = 7,5 \text{ kN}$
- 3.16.  $\delta_{AB} = 10,586 \text{ mm}$
- 3.17. Satisfaz exigências tanto de tensão quanto de deformação
- 3.18.  $d_{AB} = 3,54 \text{ mm}, d_{AC} = 3,23 \text{ mm},$   
 $L_{AB} = 750,49 \text{ mm}$
- 3.19.  $P = 65,63 \text{ kN}$
- 3.20.  $A_{BC} = 571,43 \text{ mm}^2, A_{AB} = 142,86 \text{ mm}^2$
- 3.21.  $\alpha = 0,708^\circ$
- 3.22.  $P = 11,3 \text{ kN}$
- 3.23.  $\delta_{AB} = 3,970 \text{ mm}$
- 3.24.  $w = 3,40 \text{ kN/m}$
- 3.25.  $T = 4,50 \text{ kN}$
- 3.26.  $\delta = 0,126 \text{ mm}, \Delta d = -0,00377 \text{ mm}$
- 3.27.  $\epsilon_y = -0,01500 \text{ mm/mm}, \gamma_{xy} = -0,00524 \text{ rad},$   
 $\epsilon_x = 0,00540 \text{ mm/mm}$
- 3.28.  $d' = 38,0861 \text{ mm}$
- 3.29.  $\nu = 0,300$
- 3.30.  $L = 50,0377 \text{ mm}, d = 12,99608 \text{ mm}$
- 3.31.  $E = 227.500 \text{ MPa}, P = 9,896 \text{ kN}$
- 3.33.  $p = 741 \text{ kPa}, \delta = 7,41 \text{ mm}$
- 3.34.  $\epsilon_x = 0,00750 \text{ mm/mm}, \gamma_{xy} = 0,01222 \text{ rad},$   
 $\epsilon_y = -0,00375 \text{ mm/mm}$
- 3.35.  $G = 31,60 \text{ GPa}$
- 3.36.  $d' = 12,4716 \text{ mm}$
- 3.37.  $\epsilon = 0,0010186 \text{ mm/mm}, \text{deformação } \epsilon = 0$
- 3.38.  $\delta L_{AB} = 2,1171 \text{ mm}$
- 3.39.  $P = 0,885 \text{ kN}$
- 3.40.  $L = 69,806 \text{ mm}$
- 3.41.  $\epsilon_p = 0,00227 \text{ mm/mm}, \epsilon_t = 0,000884 \text{ mm/mm}$
- 3.42.  $E_{\text{aprox}} = 250 \text{ GPa}$
- 3.43.  $u_t = 118(10^6) \frac{\text{N}}{\text{m}^2}$

Capítulo 4

- 4.1.  $\delta_A = -3,64(10^{-3}) \text{ mm}$
- 4.2.  $\delta_{AB} = -1,74769 \text{ mm}$
- 4.3.  $P_1 = 304,69 \text{ kN}, P_2 = 609,38 \text{ kN}$
- 4.4.  $(\delta_A)_D = 3,8483 \text{ mm}$
- 4.5.  $\delta_B = 2,31 \text{ mm}, \delta_A = 2,64 \text{ mm}$

$$\begin{aligned}
4.6. \quad & P_1 = 70,46 \text{ kN}, P_2 = 152,27 \text{ kN} \\
4.7. \quad & p = 21,8 \text{ MPa}, \delta_{BC} = 1,13 \text{ mm}, \delta_{BA} = 0 \\
4.8. \quad & \delta_1 = 0,736 \text{ mm} \\
4.9. \quad & \alpha_{DC} = 0,0039^\circ, \beta_{AB} = 0,0334^\circ \\
4.10. \quad & \delta_A = 2,990 \text{ mm} \\
4.11. \quad & \delta_F = 0,34 \text{ mm} \\
4.12. \quad & \alpha_{AC} = 0,00143^\circ \\
4.13. \quad & \delta_{\text{tot}} = 33,87 \text{ mm} \\
4.14. \quad & W = 9,69 \text{ kN} \\
4.15. \quad & \delta_F = 2,23 \text{ mm} \\
4.16. \quad & \delta_B = 12,37 \text{ mm} \\
4.17. \quad & P = 50,47 \text{ kN} \\
4.19. \quad & \delta_D = 17,3 \text{ mm} \\
4.20. \quad & d_{CD} = 12,887 \text{ mm}, d_{AB} = 22,321 \text{ mm} \\
4.21. \quad & w = 13,41 \text{ kN/m}, x = 1,35 \text{ m} \\
& \text{Hastes } AB \text{ e } CD \text{ falham simultaneamente.} \\
4.22. \quad & F = 12,0 \text{ kN}, \delta_{A/B} = -0,864 \text{ mm} \\
4.23. \quad & F = 17,0 \text{ kN}, \delta_{A/B} = -1,03 \text{ mm} \\
4.25. \quad & \delta = \frac{PL}{\pi E r_2 r_1} + \frac{\gamma L^2 (r_2 + r_1)}{6E(r_2 - r_1)} - \frac{\gamma L^2 r_1^2}{3Er_2(r_2 - r_1)} \\
4.26. \quad & \delta = \frac{0,511P}{\pi r_0 E} \\
4.27. \quad & \delta = \frac{2,63P}{\pi r E} \\
4.29. \quad & \delta = \frac{\gamma L^2}{6E} \\
4.30. \quad & \delta = 0,1804 \text{ mm} \\
4.31. \quad & \sigma_{aço} = 24,323 \text{ MPa}, \sigma_{\text{conc}} = 3,527 \text{ MPa} \\
4.32. \quad & d_{aço} = 44,95 \text{ mm} \\
4.33. \quad & \sigma_{\text{al}} = 27,5 \text{ MPa}, \sigma_{aço} = 79,9 \text{ MPa} \\
4.34. \quad & \sigma_{aço} = 65,9 \text{ MPa}, \sigma_{\text{conc}} = 8,24 \text{ MPa} \\
4.35. \quad & d = 33,9 \text{ mm} \\
4.37. \quad & \sigma_{aço} = 5,335 \text{ MPa}, \sigma_{\text{lat}} = 2,792 \text{ MPa}, \\
4.38. \quad & d_{aço} = 58,88 \text{ mm} \\
4.39. \quad & T_{AC} = 1,249 \text{ kN}, T_{AB} = 6,251 \text{ kN} \\
4.40. \quad & A_{AB} = 3,60911 \text{ mm}^2 \\
4.41. \quad & P = F_{\text{lat}} = 198 \text{ kN} \\
4.42. \quad & T_{AB} = 1,469 \text{ kN}, T_{A'B'} = 1,781 \text{ kN} \\
4.43. \quad & P_b = 14,4 \text{ kN} \\
4.45. \quad & w = 45,9 \text{ kN/m} \\
4.46. \quad & \sigma_D = 13,4 \text{ MPa}, \sigma_{BC} = 9,55 \text{ MPa} \\
4.47. \quad & \theta = 63,7(10^{-6}) \text{ rad} \\
4.49. \quad & d_{AC} = 1,79 \text{ mm} \\
4.50. \quad & \sigma_{AB} = \frac{7P}{12A}, \sigma_{CD} = \frac{P}{3A}, \sigma_{EF} = \frac{P}{12A}
\end{aligned}$$

$$\begin{aligned}
4.51. \quad & P = 1,16 \text{ kN} \\
4.53. \quad & \sigma_{aço} = 102 \text{ MPa}, \sigma_{\text{lat}} = 50,9 \text{ MPa} \\
4.54. \quad & P = 126 \text{ kN} \\
4.55. \quad & T_{AB} = T_{CD} = 16,7 \text{ kN}, T_{EF} = 33,3 \text{ kN} \\
4.56. \quad & \delta_B = 0,073522 \text{ mm} \\
4.57. \quad & F_{EF} = 6,316 \text{ kN}, F_{CD} = 1.053 \text{ kN} \\
4.58. \quad & F_1 = \left( \frac{A_1 E_1}{2A_1 E_1 + A_2 E_2} \right) P, \\
& F_2 = \left( \frac{A_2 E_2}{2A_1 E_1 + A_2 E_2} \right) P \\
4.59. \quad & A'_1 = \left( \frac{E_1}{E_2} \right) A_1 \\
4.61. \quad & F_B = 0,2712 \text{ kN}, F_C = 0,8136 \text{ kN}, F_D = 1,8983 \text{ kN} \\
4.62. \quad & \delta_D = 0,003867 \text{ mm} \\
4.63. \quad & F_A = F_B = 25,6 \text{ kN} \\
4.65. \quad & F_{AB} = 12,0 \text{ kN (T)}, F_{AC} = F_{AD} = 6,00 \text{ kN (C)} \\
4.66. \quad & F_B = 16,9 \text{ kN}, F_A = 16,9 \text{ kN} \\
4.67. \quad & \delta_{\text{esp}} = 0,0390 \text{ mm} \\
4.68. \quad & T_{BC} = 45,2804 \text{ kN}, T_{DC} = 135,8411 \text{ kN} \\
4.69. \quad & \Delta\theta = 0,180^\circ \\
4.70. \quad & s = 0,7425 \text{ mm} \\
4.71. \quad & L' = 139,056 \text{ m} \\
4.72. \quad & \sigma_{\text{al}} = 15,05 \text{ MPa}, \sigma_{\text{lat}} = 33,85 \text{ MPa}, \\
& \sigma_{aço} = 135,41 \text{ MPa} \\
4.73. \quad & T_1 = 55,45^\circ\text{C}, \sigma = 1,45 \text{ MPa} \\
4.74. \quad & F = 489,03 \text{ kN} \\
4.75. \quad & F = 477,29 \text{ kN} \\
4.76. \quad & \Delta_{\text{folga}} = 8,640 \text{ mm}, F = 76,80 \text{ kN} \\
4.77. \quad & T' = 45,77^\circ\text{C}, F = 61,958 \text{ kN}, \sigma = 87,65 \text{ MPa} \\
4.78. \quad & \sigma = 185,58 \text{ MPa}, L'_{\text{al}} = 200,117793 \text{ mm} \\
4.79. \quad & F = 6,99 \text{ kN} \\
4.81. \quad & F_{AB} = F_{EF} = 1,85 \text{ kN} \\
4.82. \quad & \sigma = 134,40 \text{ MPa} \\
4.83. \quad & F = 18,566 \text{ kN} \\
4.84. \quad & \sigma_{aço} = 24,68 \text{ MPa}, \sigma_{\text{lat}} = 30,64 \text{ MPa} \\
4.85. \quad & F = \frac{\alpha A E}{2} (T_B - T_A) \\
4.86. \quad & F = 2,442 \text{ kN} \\
4.87. \quad & \sigma_{\text{máx}} = 190 \text{ MPa} \\
4.89. \quad & P = 44,1 \text{ kN} \\
4.90. \quad & P = 5,4 \text{ kN}
\end{aligned}$$

- 4.91.  $\sigma_{\text{máx}} = 217,78 \text{ MPa}$   
 4.93.  $P = 19 \text{ kN}$ ,  $K = 1,26$   
 4.94.  $P = 72,00 \text{ kN}$ ,  $\sigma_{\text{méd}} = 45,00 \text{ MPa}$ ,  $K = 1,60$   
 4.95.  $P = 77,1 \text{ kN}$ ,  $\delta = 0,429 \text{ mm}$   
 4.96.  $\sigma_{\text{aço}} = 250 \text{ MPa}$ ,  $\sigma_{\text{al}} = 171,31 \text{ MPa}$   
 4.97.  $P = 126 \text{ kN}$   
 4.98. a)  $F_{\text{aço}} = 444 \text{ N}$ ,  $F_{\text{al}} = 156 \text{ N}$ ;  
 b)  $F_{\text{aço}} = 480 \text{ N}$ ,  $F_{\text{al}} = 240 \text{ N}$   
 4.99.  $\Delta\sigma_{AB} = 60 \text{ MPa (T)}$ ,  $\Delta\sigma_{BC} = 60 \text{ MPa (T)}$   
 4.100.  $\delta_{\text{Total}} = 18,286 \text{ mm}$   
 4.101.  $w = 21,9 \text{ kN/m}$ ,  $\delta_G = 4,24 \text{ mm}$   
 4.102. a)  $w = 18,7 \text{ kN/m}$ , b)  $w = 21,9 \text{ kN/m}$   
 4.103. a)  $P = 92,8 \text{ kN}$ , b)  $P = 181 \text{ kN}$   
 4.105.  $w = 2,00 \text{ kN/m}$ ,  $\delta = 1,500 \text{ mm}$   
 4.106.  $\delta = \frac{\gamma^2 L^3}{3c^2}$   
 4.107.  $\delta = \frac{3}{5} \left( \frac{\gamma}{c} \right)^{\frac{2}{3}} L^{\frac{5}{3}}$   
 4.108.  $P = 549,78 \text{ kN}$ ,  $\Delta\delta = 0,180 \text{ mm} \leftarrow$   
 4.109.  $P = 549,78 \text{ kN}$ ,  $\delta_C' = 0,300 \text{ mm}$   
 4.110.  $F = 64,189 \text{ kN}$ . Sim, porque conforme o rebite esfria, as chapas e as cabeças do rebite também se deformarão. A força  $F_T$  no rebite não será tão grande.  
 4.111.  $P = 22,5 \text{ kN}$   
 4.112.  $F_C = 0,974 \text{ kN}$ ,  $F_B = 0,433 \text{ kN}$   
 4.114.  $F_B = 8,526 \text{ kN}$ ,  $F_A = 8,606 \text{ kN}$   
 4.115.  $P = 19,776 \text{ kN}$   
 4.116.  $\sigma_{\text{aço}} = 13,23 \text{ MPa}$ ,  $\sigma_c = 1,92 \text{ MPa}$ ,  $\delta = 0,15881 \text{ mm}$   
 4.117.  $A_{\text{aço}} = 11,397,38 \text{ mm}^2$ ,  $\delta = 0,15793 \text{ mm}$   
 4.118.  $\delta_D = 1,17 \text{ mm}$   
 4.119.  $\delta_{A/B} = 0,491 \text{ mm}$

## Capítulo 5

- 5.1. a)  $T = 0,87 \text{ kN}\cdot\text{m}$  b)  $T' = 0,87 \text{ kN}\cdot\text{m}$   
 5.2.  $r' = 0,841r$   
 5.3.  $r' = 0,707r$   
 5.5.  $\tau_{\text{máx}} = 75,5 \text{ MPa}$   
 5.6.  $\tau_C = 28,75 \text{ MPa}$ ,  $\tau_D = -11,66 \text{ MPa}$   
 5.7.  $\tau_{\text{máx}} = 45,82 \text{ MPa}$   
 5.8.  $\tau_{\text{máx}} = 45,82 \text{ MPa}$ ,  $\tau_p = 35,80 \text{ MPa}$   
 5.9.  $\tau_{AB} = 62,55 \text{ MPa}$ ,  $\tau_{BC} = 18,89 \text{ MPa}$   
 5.10.  $\tau_{\text{máx}} = 14,5 \text{ MPa}$

- 5.11.  $\tau_{\text{máx}} = 11,9 \text{ MPa}$   
 5.13.  $d_i = 60 \text{ mm}$   
 5.14.  $T_1 = 215 \text{ N}\cdot\text{m}$ ,  $(\tau_{\text{máx}})_{CD} = 4,00 \text{ MPa}$ ,  
 $(\tau_{\text{máx}})_{DE} = 2,58 \text{ MPa}$   
 5.15.  $\tau_{\text{máx}} = 5,38 \text{ MPa}$   
 5.17.  $(\tau_{EA})_{\text{máx}} = 5,66 \text{ MPa}$ ,  $(\tau_{CD})_{\text{máx}} = 8,91 \text{ MPa}$   
 5.18.  $\tau_A = 13,79 \text{ MPa}$ ,  $\tau_B = 24,14 \text{ MPa}$   
 5.19.  $\tau_C = 28,73 \text{ MPa}$   
 5.21.  $\tau_{\text{máx}} = 0$  ocorre em  $x = 0,700 \text{ m}$ .  
 $\tau_{\text{máx}} = 33,0 \text{ MPa}$  ocorre em  $x = 0$ . Entretanto, por conta do princípio de Saint-Venant, a  $\tau_{\text{máx}}$  obtida *não é válida*.  
 5.22.  $d = 34,4 \text{ mm}$ . Entretanto, a análise *não é válida* por conta do princípio de Saint Venant.  
 5.23.  $\tau_{\text{méd}} = 1,17 \text{ MPa}$   
 5.24.  $\tau_A = 159,15 \text{ MPa}$   
 5.25.  $\tau_B = 159,15 \text{ MPa}$   
 5.27.  $t_0 = 133 \text{ N}\cdot\text{m/m}$ ,  $\tau_A = 0,255 \text{ MPa}$ ,  
 $\tau_B = 0,141 \text{ MPa}$   
 5.29.  $T_0 = 670 \text{ N}\cdot\text{m}$ ,  $\tau_{\text{máx}} = 6,66 \text{ MPa}$   
 5.30.  $\tau_{\text{máx}} = \frac{2TL^3}{\pi[r_A(L-x) + r_Bx]^3}$   
 5.31.  $T_B = \frac{2T_A + t_AL}{2}$ ;  $\tau_{\text{máx}} = \frac{(2T_A + t_AL)r_o}{\pi(r_o^4 - r_i^4)}$   
 5.32.  $t = 5,17 \text{ mm}$   
 5.33.  $t = 2,998 \text{ mm}$   
 5.34.  $\tau_{\text{máx}} = 9,382 \text{ MPa}$   
 5.35.  $d = 15 \text{ mm}$   
 5.36.  $t = 3,427 \text{ mm}$   
 5.37.  $\tau_{\text{máx}} = 46,055 \text{ MPa}$   
 5.38.  $d = 20 \text{ mm}$   
 5.39.  $(\tau_{AB})_{\text{máx}} = 1,04 \text{ MPa}$ ,  $(\tau_{BC})_{\text{máx}} = 3,11 \text{ MPa}$   
 5.40.  $\tau_{\text{máx}} = 48,634 \text{ MPa}$   
 5.41.  $d_A = 12,4 \text{ mm}$ ,  $d_B = 16,8 \text{ mm}$   
 5.42.  $\omega = 3.135,714 \text{ rpm}$   
 5.43.  $d = 35 \text{ mm}$   
 5.45. Aumento percentual na tensão de torção =  
 % aumento em  $\phi = 6,67\%$   
 5.46.  $d_i = 201 \text{ mm}$ ,  $\phi = 3,30^\circ$   
 5.47.  $\phi_{A/D} = 0,879^\circ$   
 5.49.  $\tau_{\text{máx}} = 20,797 \text{ MPa}$ ,  $\phi = 4,766^\circ$   
 5.50.  $\phi_{C/D} = 0,243^\circ$   
 5.51.  $\phi_B = 5,74^\circ$
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